

Chapter 9. Behavior of Solutions

§ 9-1 Introduction	2
§ 9-2 Raoult's Law and Henry's Law	2
§ 9-3 Activity of a component in solution	3
§ 9-4 Gibbs-Duhem Equation	4
§ 9-5 Gibbs Free Energy of a Binary Solution.....	4
§9-6 Properties of Ideal Solution	7
§ 9-7 Nonideal solution.....	10
§ 9-8 Applications of Gibbs-Duhem Equation.....	11
§ 9-9 Regular Solution	19
§ 9-10 Statistical (Quasi-chemical) Model of Solution .	22
§ 9-11 Subregular Solution	25

§ 9-1 Introduction

1. Mixing of real gases:

T , P , \Rightarrow Ideal gas mixture.

2. Condensed phases (Liquid or Solid solution)

- Strong interaction between atoms.
- Solid solubility depends on: 1) atomic size ratio
2) electronegativity
3) e/a ratio (valence)

§9-2 Raoult's Law and Henry's Law

1. Pure A liquid (solid)

At temperature T , saturated vapor pressure : p_A^o

Rate of evaporation : $r_e(A)$

Condensation rate : $r_c(A) = k p_A^o$

At equilibrium : $r_e(A) = r_c(A) = k p_A^o$

2. Pure B liquid or solid: $r_e(B) = r_c(B) = k' p_B^o$

3. Liquid + small amount of B

At T , saturated vapor pressure : p_A , p_B

Condensation rate of A, B : $r_c(A) = k p_A$, $r_c(B) = k' p_B$

Assumptions: * evaporation of A, B are independent of composition.

i.e. same bond energy: $E_{AA} = E_{BB} = E_{AB}$ (ideal case)

* surface composition = bulk composition

* Fraction of surface occupied by A = X_A

Evaporation rate of A: $r_e(A) \cdot X_A$

At equilibrium : $r_e(A) \cdot X_A = r_c(A) = k p_A$

$k p_A^o \cdot X_A = k p_A$

$$\begin{cases} p_A = X_A p_A^o \\ p_B = X_B p_B^o \end{cases} \Rightarrow \text{Raoult's Law}$$

4. If E_{AB} is more negative, and A (solute) in B (solvent), A is surrounded by B

$$\Rightarrow r_e(A) \quad r'_e(A)$$

$$r'_e(A) < r_e(A)$$

$$r'_e(A) \cdot X_A = r_c(A) = k p_A$$

$$\frac{r'_e(A) \cdot X_A}{r_e(A)} = \frac{k p_A}{k p_A^o}$$

$$p_A = \frac{r'_e(A)}{r_e(A)} \cdot X_A \cdot p_A^o$$

$$\left\{ \begin{array}{l} p_A = \gamma_A \cdot X_A \cdot p_A^o \quad (\text{eq.1}) \\ p_B = \gamma_B \cdot X_B \cdot p_B^o \quad (\text{eq.2}) \end{array} \right. \Rightarrow \text{Henry's Law}$$

$$\gamma_A < 1 \text{ and indep. of comp. } \quad \gamma_A = \text{constant}$$

$$\gamma_B < 1 \text{ and indep. of comp. } \quad \gamma_B = \text{constant}$$

- When X_A ; at same point, A is not only surrounded by B, then

$$r'_e(A) \text{ varies with composition}$$

$$\gamma_A \text{ is not a constant (it depends on composition)}$$

- (eq.1) is obeyed only over an initial range of concentration of A dissolved in B
- (eq.2) is obeyed only over an initial range of concentration of B dissolved in A

$$\gamma_A < 1, \quad \gamma_B < 1 \quad \Leftrightarrow \text{negative deviation}$$

- If E_{AB} is less negative, then $r'_e(A) > r_e(A)$

$$\frac{r'_e(A)}{r_e(A)} = \gamma_A > 1 \quad \Leftrightarrow \text{positive deviation.}$$

§9-3 Activity of a component in solution

$$a_i \equiv \frac{f_i}{f_i^o}$$

If the vapor is ideal gas, $f_i = p_i$

$$a_i = \frac{p_i}{p_i^o}$$

Raoult's Law

$$\begin{cases} p_A = X_A \cdot p_A^o, & a_A = X_A \\ p_B = X_B \cdot p_B^o, & a_B = X_B \end{cases}$$

Raoult's Law: $a_i = X_i, \gamma_i = 1$

$$\text{Henry's Law} \begin{cases} p_A = \gamma_A \cdot X_A \cdot p_A^o, & a_A = \gamma_A \cdot X_A \\ p_B = \gamma_B \cdot X_B \cdot p_B^o, & a_B = \gamma_B \cdot X_B \end{cases}$$

Henry's Law: $a_i = \gamma_i X_i, \gamma_i = 1$
and γ_i is a constant, indep. of composition.

§9-4 Gibbs-Duhem Equation

In a solution: ($n_i + n_j + n_k + \dots$)

$Q' = Q'(T, P, n_i, n_j, n_k, \dots)$, at constant T, P :

$$dQ' = \left(\frac{\partial Q'}{\partial n_i} \right)_{T, P, n_j, \dots} \cdot dn_i + \left(\frac{\partial Q'}{\partial n_j} \right)_{n_i, T, P, \dots} \cdot dn_j + \dots$$

$$\bar{Q}_i \equiv \left(\frac{\partial Q'}{\partial n_i} \right)_{T, P, n_j, \dots}, \text{ Partial Molar Quantity}$$

$$dQ' = \bar{Q}_i dn_i + \bar{Q}_j dn_j + \bar{Q}_k dn_k + \dots$$

$$Q' = n_i \bar{Q}_i + n_j \bar{Q}_j + \dots$$

$$dQ' = (\bar{Q}_i dn_i + \bar{Q}_j dn_j + \dots) + (n_i d\bar{Q}_i + n_j d\bar{Q}_j + \dots)$$

$$n_i d\bar{Q}_i + n_j d\bar{Q}_j + \dots = 0$$

$$\text{or} \begin{cases} \sum n_i d\bar{Q}_i = 0 \\ \sum X_i d\bar{Q}_i = 0 \end{cases} \Rightarrow \text{Gibbs-Duhem Eq.}$$

§9-5 Gibbs Free Energy of a Binary Solution

- 1.
2. $\left\{ \begin{array}{l} \text{Molar Gibbs free energy: } (G) \\ \text{Partial molar Gibbs free energy: } (\overline{G}_A, \overline{G}_B) \end{array} \right.$

$$G' = n_A \overline{G}_A + n_B \overline{G}_B$$

or $G = X_A \overline{G}_A + X_B \overline{G}_B \dots\dots\dots(1)$

$$dG = (X_A d\overline{G}_A + X_B d\overline{G}_B) + (\overline{G}_A dX_A + \overline{G}_B dX_B)$$

$$dG = \overline{G}_A dX_A + \overline{G}_B dX_B$$

$$X_A + X_B = 1 \quad dX_A = -dX_B$$

$$dG = \overline{G}_A dX_A - \overline{G}_B dX_A = (\overline{G}_A - \overline{G}_B) dX_A$$

$$\frac{dG}{dX_A} = \overline{G}_A - \overline{G}_B$$

$$X_B \frac{dG}{dX_A} = X_B \overline{G}_A - X_B \overline{G}_B \dots\dots\dots(2)$$

$$(1)+(2) \quad G + X_B \frac{dG}{dX_A} = (X_A + X_B) \overline{G}_A = \overline{G}_A$$

$$\left\{ \begin{array}{l} \overline{G}_A = G + (1 - X_A) \frac{dG}{dX_A} \\ \overline{G}_B = G + (1 - X_B) \frac{dG}{dX_B} \end{array} \right.$$

2. $\Delta G^M (\Delta \overline{G}_i^M)$:

change in Gibbs Free Energy due to formation of solution

* one mole pure i (p_i^o) \Rightarrow solution (p_i)

$$\Delta G_i = G_{i \text{ (solution)}} - G_{i \text{ (pure)}} = RT \ln \left(\frac{p_i}{p_i^o} \right)$$

$$\therefore \Delta G_i = RT \ln a_i$$

$$\left\{ \begin{array}{l} \bar{G}_i = G_i \text{ (solution)}, \quad G_i^\circ = G_i \text{ (pure)} \\ \Delta G_i = \Delta \bar{G}_i^M = \bar{G}_i - G_i^\circ \end{array} \right.$$

$$\therefore \boxed{\Delta \bar{G}_i^M = \bar{G}_i - G_i^\circ = RT \ln a_i}$$

* ($n_A + n_B$) at constant T, P

Before mixing, $G'_{\text{before}} = n_A G_A^\circ + n_B G_B^\circ$

After mixing, $G'_{\text{after}} = n_A \bar{G}_A + n_B \bar{G}_B$

$$\Delta G^M = (n_A \bar{G}_A + n_B \bar{G}_B) - (n_A G_A^\circ + n_B G_B^\circ)$$

$$= n_A (\bar{G}_A - G_A^\circ) + n_B (\bar{G}_B - G_B^\circ)$$

$$\Delta G^M = n_A \Delta \bar{G}_A^M + n_B \Delta \bar{G}_B^M$$

or $\Delta G^M = RT(n_A \ln a_A + n_B \ln a_B)$

Total one mole: $X_A + X_B = 1$

$$\left\{ \begin{array}{l} \Delta G^M = X_A \Delta \bar{G}_A^M + X_B \Delta \bar{G}_B^M \\ \text{or } \Delta G^M = RT(X_A \ln a_A + X_B \ln a_B) \end{array} \right.$$

3. Method of Tangential Intercept (圖解法求 $\Delta \bar{G}_A^M, \Delta \bar{G}_B^M$)

Given $\Delta G^M(X_B) \Rightarrow$ solve $\Delta \bar{G}_A^M$ and $\Delta \bar{G}_B^M$

$$\ominus \bar{G}_A = G + (1 - X_A) \frac{dG}{dX_A}$$

$$\bar{G}_B = G + (1 - X_B) \frac{dG}{dX_B}$$

$$\therefore \Delta \bar{G}_A = \Delta G^M + (1 - X_A) \frac{d\Delta G^M}{dX_A} \dots\dots\dots(1)$$

$$\Delta \bar{G}_B = \Delta G^M + (1 - X_B) \frac{d\Delta G^M}{dX_B} \dots\dots\dots(2)$$

Given $\Delta G^M(X_B)$, Fig. 9-1

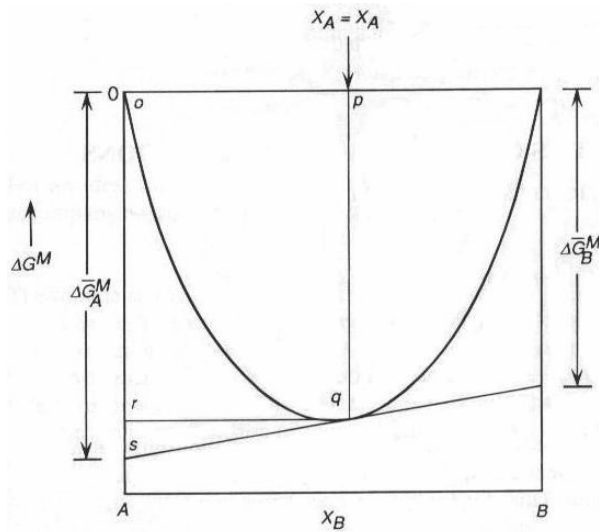


Figure 9.1 The variation , with composition , of the molar Gibbs free energy of formation of a binary solution

At composition $X_B = X_B^0 = op$, $\Delta G^M = -pq = -uw$

$$\text{Tangent at } q, \text{ slope} = \frac{d\Delta G^M}{dX_B} = \frac{rs}{rq} = \frac{vw}{qw}$$

$$\begin{aligned} \text{From (2)} \quad \Delta \overline{G}_B &= -pq + (1 - X_B^0) \frac{vw}{qw} = -uw + qw \frac{vw}{qw} = -uw + vw \\ &= -(uw - vw) = -uv \\ &= \text{tangential intercept at } X_B = 1 \end{aligned}$$

$$\begin{aligned} \text{From (1)} \quad \Delta \overline{G}_A &= -pq + (1 - X_A^0) \frac{d\Delta G^M}{dX_A} = -pq - X_B^0 \frac{d\Delta G^M}{dX_B} \\ &= -pq - rq \frac{rs}{rq} = -(pq + rs) = -(or + rs) = -os \\ &= \text{tangential intercept at } X_A = 1, (X_B = 0) \end{aligned}$$

§-6 Properties of Ideal Solution

1. Ideal solution (Raoultian Solution)

$$a_i = X_i \quad \gamma_i = 1$$

$$\Delta G^{M, id} = RT(X_A \ln X_A + X_B \ln X_B)$$

$$\left\{ \begin{aligned} \overline{\Delta G}_A^{M, id} &= RT \ln X_A \\ \overline{\Delta G}_B^{M, id} &= RT \ln X_B \end{aligned} \right.$$

$$2. \Delta V^{M,id}=0, \quad \Delta \bar{V}_i^{M,id}=0, \quad (\bar{V}_i = V_i^o)$$

$$\Theta \left(\frac{\partial G}{\partial P} \right)_{T,comp} = V, \quad \therefore \left(\frac{\partial \bar{G}_i}{\partial P} \right)_{T,comp} = \bar{V}_i$$

$$\therefore \left[\frac{\partial (\bar{G}_i - G_i^o)}{\partial P} \right]_{T,comp} = (\bar{V}_i - V_i^o)$$

$$\text{i.e.} \left[\frac{\partial \Delta \bar{G}_i^M}{\partial P} \right]_{T,comp} = \Delta \bar{V}_i^M$$

$$\Theta \quad \Delta \bar{G}_i^M = RT \ln a_i = RT \ln X_i$$

$$\therefore \Delta \bar{V}_i^M = 0, \quad \text{i.e.} \quad \bar{V}_i = V_i^o$$

$$\therefore \Delta V^{M,id} = \sum X_i \Delta \bar{V}_i^M = X_A \Delta \bar{V}_A^M + X_B \Delta \bar{V}_B^M = 0$$

$$3. \Delta H^{M,id}=0, \quad \Delta \bar{H}_i^{M,id}=0 \quad (\bar{H}_i = H_i^o)$$

$$\Theta \quad \left[\frac{\partial (G/T)}{\partial T} \right]_{P,comp} = - \frac{H}{T^2}$$

$$\therefore \left[\frac{\partial (\bar{G}_i/T)}{\partial T} \right]_{P,comp} = - \frac{\bar{H}_i}{T^2}$$

$$\therefore \left[\frac{\partial \left(\frac{\bar{G}_i - G_i^o}{T} \right)}{\partial T} \right]_{P,comp} = - \frac{(\bar{H}_i - H_i^o)}{T^2}$$

$$\therefore \left[\frac{\partial (\Delta \bar{G}_i^M / T)}{\partial T} \right]_{P,comp} = - \frac{\Delta \bar{H}_i^M}{T^2}$$

$$\Theta \quad \Delta \bar{G}_i^M = RT \ln a_i = RT \ln X_i$$

$$\therefore \left[\frac{\partial (R \ln X_i)}{\partial T} \right]_{P,comp} = 0$$

$$\Delta \bar{H}_i^M = 0, \quad (\bar{H}_i = H_i^\circ)$$

$$\therefore \Delta H^{M,id} = \sum X_i \Delta \bar{H}_i^M = 0$$

$$4. \quad \begin{cases} \Delta S^{M,id} = -R(X_A \ln X_A + X_B \ln X_B) \\ \Delta \bar{S}_i^{M,id} = -R \ln X_i \end{cases}$$

$$\Theta \left(\frac{\partial G}{\partial T} \right)_{P,comp} = -S \quad \left[\frac{\partial(\Delta G^M)}{\partial T} \right]_{P,comp} = -\Delta S^M$$

$$\Theta \Delta G^{M,id} = RT \sum X_i \ln X_i = RT(X_A \ln X_A + X_B \ln X_B)$$

$$\therefore \Delta S^{M,id} = -R \sum X_i \ln X_i = -R(X_A \ln X_A + X_B \ln X_B)$$

$$\text{又 } \Theta \Delta S^M = \sum X_i \Delta \bar{S}_i^M = (X_A \Delta \bar{S}_A^M + X_B \Delta \bar{S}_B^M)$$

$$\therefore \Delta \bar{S}_A^{M,id} = -R \ln X_A, \quad \Delta \bar{S}_B^{M,id} = -R \ln X_B$$

Notes: (1) $\Delta S^{M,id}$ is indep. of temperature

(2) $\Delta S^{M,id}$ is the entropy increase due to configurational entropy change

⊗ consider: (N_A A atoms + N_B B atoms)

$$\begin{aligned} \therefore \Delta S'_{conf.} &= k \ln \frac{(N_A + N_B)!}{N_A! N_B!} \\ &= k [\ln(N_A + N_B)! - \ln N_A! - \ln N_B!] \\ &= k [(N_A + N_B) \ln(N_A + N_B) - (N_A + N_B)] \\ &\quad - (N_A \ln N_A - N_A) - (N_B \ln N_B - N_B) \\ &= -k \left[N_A \ln \left(\frac{N_A}{N_A + N_B} \right) + N_B \ln \left(\frac{N_B}{N_A + N_B} \right) \right] \end{aligned}$$

$$\Theta \frac{N_A}{N_A + N_B} = X_A, \quad \frac{N_B}{N_A + N_B} = X_B$$

$$\therefore \Delta S'_{conf.} = -k(N_A + N_B)[X_A \ln X_A + X_B \ln X_B] \quad \Theta \frac{(N_A + N_B)}{N_O} = n$$

$$\therefore \Delta S'_{conf.} = -n N_O k (X_A \ln X_A + X_B \ln X_B) = -nR (X_A \ln X_A + X_B \ln X_B)$$

$$\text{one mole } \therefore \Delta S_{conf.} = -R(X_A \ln X_A + X_B \ln X_B) = \Delta S^{M,id}$$

§ 9-7 Nonideal solution

Activity coefficient: $\gamma_i = \frac{a_i}{X_i}$

$$\left\{ \begin{array}{l} \gamma_i = 1 \quad , \text{ ideal solution} \\ \gamma_i \neq 1 \quad , \text{ nonideal solution} \end{array} \right. \quad \begin{array}{l} \gamma_i > 1 \quad : \text{ positive deviation} \\ \gamma_i < 1 \quad : \text{ negative deviation} \end{array}$$

$$\ominus \left[\frac{\partial(\Delta \overline{G}_i^M / T)}{\partial T} \right]_{P, \text{Comp}} = \frac{-\Delta \overline{H}_i^M}{T^2}$$

$$\Delta \overline{G}_i^M = RT \ln a_i = RT (\ln \gamma_i + \ln X_i)$$

$$d\left(\frac{1}{T}\right) = \frac{-dT}{T^2}$$

$$\therefore \left[\frac{\partial(\Delta \overline{G}_i^M / T)}{\partial(1/T)} \right]_{P, \text{Comp}} = \Delta \overline{H}_i^M$$

$$\therefore \boxed{\left[\frac{\partial(R \ln \gamma_i)}{\partial(1/T)} \right]_{P, \text{Comp}} = \Delta \overline{H}_i^M}$$

Notes : (1) If $\gamma_i = \text{constant}$ (indep. of T), $\Delta \overline{H}_i^M = 0$

If $\gamma_i(T) \quad \Delta \overline{H}_i^M \neq 0$

(2) $T \uparrow \Rightarrow$ Nonideal solution \rightarrow ideal solution ($\gamma_i \rightarrow 1$)

(3) \otimes Positive deviation : $\gamma_i > 1$

when $T \uparrow$, $\left(\frac{1}{T}\right) \downarrow \Rightarrow \gamma_i \rightarrow 1$, $\therefore \gamma_i \downarrow$

$$\therefore \left(\frac{d\gamma_i}{dT}\right) < 0$$

$$\therefore \Delta \overline{H}_i^M = \left[\frac{\partial(R \ln \gamma_i)}{\partial(1/T)} \right]_{P, \text{Comp}} > 0$$

\therefore Mixing process is endothermic.

\otimes negative deviation : $\gamma_i < 1$

$$\left(\frac{d\gamma_i}{dT}\right) > 0, \quad \Delta\overline{H}_i^M < 0$$

∴ Mixing process is exothermic.

(4) ⊗ Positive deviation : $\gamma_i > 1$, $\left(\frac{d\gamma_i}{dT}\right) < 0$

endothermic : $\Delta\overline{H}_i^M > 0$

i.e. A-B bond energy is less negative

∴ E_{AA} , E_{BB} more negative ⇒ clustering

⊗ negative deviation : $\gamma_i < 1$, $\Delta\overline{H}_i^M < 0$, $\left(\frac{d\gamma_i}{dT}\right) > 0$

A-B bond energy is more negative

⇒ ordering , (formation of compound)

§ 9-8 Applications of Gibbs-Duhem Equation

1. Given $a_B(X_B)$, calculate a_A

- In a binary solution , usually only activity of one component is measured , the other can be calculated.

$$\sum X_i d\overline{Q}_i = 0$$

$$X_A d\Delta\overline{G}_A^M + X_B d\Delta\overline{G}_B^M = 0, \quad \Delta\overline{G}_i^M = RT \ln a$$

$$\therefore X_A d \ln a_A + X_B d \ln a_B = 0$$

$$d \ln a_A = - \frac{X_B}{X_A} d \ln a_B$$

$$\therefore \ln a_A (\text{at } X_A) = - \int_{\ln a_B \text{ at } X_A=1, X_B=0}^{\ln a_B \text{ at } X_A} \left(\frac{X_B}{X_A}\right) d \ln a_B, \quad \text{Fig . 9-2}$$

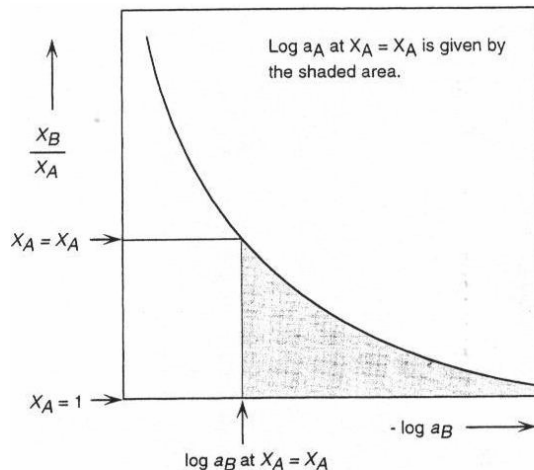


Figure 9.2 A schematic representation of the variation of $\log a_g$ with X_B/X_A in a binary solution, and illustration of the application of the Gibbs-Duhem equation to calculation of the activity of component A

Note: $\left\{ \begin{array}{l} (1) X_B \rightarrow 1, \left(\frac{X_B}{X_A}\right) \rightarrow \infty, a_B \rightarrow 1 \quad \therefore \ln a_B \rightarrow 0 \\ (2) X_B \rightarrow 0, \left(\frac{X_B}{X_A}\right) \rightarrow 0, a_B \rightarrow 0 \quad \therefore \ln a_B \rightarrow -\infty, -\ln a_B \rightarrow +\infty \end{array} \right.$

\therefore two tails exist \Rightarrow error in integrated area \Rightarrow eliminate tail error by using γ_B

$$\ominus X_A + X_B = 1$$

$$dX_A + dX_B = 0$$

$$X_A \frac{dX_A}{X_A} + X_B \frac{dX_B}{X_B} = 0$$

$$\therefore X_A d \ln X_A + X_B d \ln X_B = 0$$

$$\ominus X_A d \ln a_A + X_B d \ln a_B = 0$$

$$(X_A d \ln a_A + X_B d \ln a_B) + (X_A d \ln X_A + X_B d \ln X_B) = 0$$

$$\therefore (X_A d \ln a_A + X_B d \ln a_B) = 0$$

$$d \ln a_A = - \left(\frac{X_A}{X_B}\right) d \ln a_B$$

$$\therefore \ln a_A \text{ (at } X_A) = - \int_{\ln \gamma_B \text{ at } X_A=1, X_B=0}^{\ln \gamma_B \text{ at } X_A} \left(\frac{X_B}{X_A}\right) d \ln \gamma_B$$

when $X_B \rightarrow 0, \left(\frac{X_B}{X_A}\right) \rightarrow 0, \ln a_B \rightarrow \text{constant}, \ln a_B \rightarrow \text{constant}, \text{ Fig. 9-3.}$

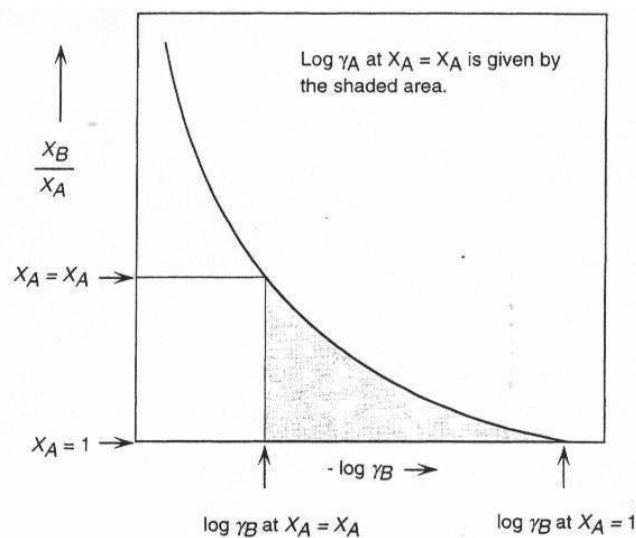


Figure 9.3 A schematic representation of the variation of $\log \gamma_B$ with X_B/X_A in a binary solution, and illustration of the application of the Gibbs-Duhem equation to calculation of the activity coefficient of component A

- The 2nd tail is eliminated by \mathbf{a} -function

Define $\mathbf{a}_i \equiv \frac{\ln \gamma_i}{(1-X_i)^2}$

When $X_B \rightarrow 1$, $X_A \rightarrow 1$, $\ln \gamma_B \rightarrow 0$ and $(1-X_B) \rightarrow 0 \Rightarrow \mathbf{a}_B$ is finite.

\therefore Given $\mathbf{a}_B \Rightarrow$ calculate \mathbf{a}_A

$$\ominus \mathbf{a}_B = \frac{\ln \gamma_B}{X_A^2}$$

$$\therefore \ln \gamma_B = \mathbf{a}_B X_A^2$$

$$d \ln \gamma_B = 2 \mathbf{a}_B X_A dX_A + X_A^2 d\mathbf{a}_B$$

$$\therefore d \ln \gamma_A = - \left(\frac{X_B}{X_A} \right) d \ln \gamma_B$$

$$= - \left(\frac{X_B}{X_A} \right) (2 \mathbf{a}_B X_A dX_A + X_A^2 d\mathbf{a}_B)$$

$$= - 2 X_B \mathbf{a}_B dX_A - X_B X_A d\mathbf{a}_B$$

$$\therefore \ln \gamma_A = - \int_{X_A=1}^{X_A} 2 X_B \mathbf{a}_B dX_A - \int_{\mathbf{a}_B \text{ at } X_A=1}^{\mathbf{a}_B} X_B X_A d\mathbf{a}_B$$

$$\ominus \int d(xy) = \int ydx + \int xdy$$

$$\Rightarrow \int X_B X_A dX_B = \int d(X_B X_A \alpha_B) - \int \alpha_B d(X_B X_A)$$

$$\Rightarrow \ln \gamma_A = - \int 2 X_B \mathbf{a}_B dX_A - [\int d(X_B X_A \alpha_B) - \int \alpha_B d(X_A X_B)]$$

$$= - \int 2 X_B \alpha_B dX_A - \int d(X_B X_A \alpha_B) + \int \alpha_B d(X_A X_B)$$

$$= - \int 2 X_B \mathbf{a}_B dX_A - X_B X_A \mathbf{a}_B + \int \alpha_B X_A dX_A + \int \alpha_B X_A dX_B$$

$$\therefore \ln \gamma_A = - \int 2 X_B \mathbf{a}_B dX_A - X_B X_A \mathbf{a}_B + \int \alpha_B X_B dX_A - \int \alpha_B X_A dX_A$$

$$= - X_B X_A \alpha_B - \int (2 X_B \mathbf{a}_B - \mathbf{a}_B X_B + \mathbf{a}_B X_A) dX_A$$

$$= - X_B X_A \alpha_B - \int (2 X_B - X_B + X_A) \alpha_B dX_A$$

$$\therefore \ln \gamma_A = - X_B X_A \mathbf{a}_B - \int_{X_A=1}^{X_A} \alpha_B dX_A$$

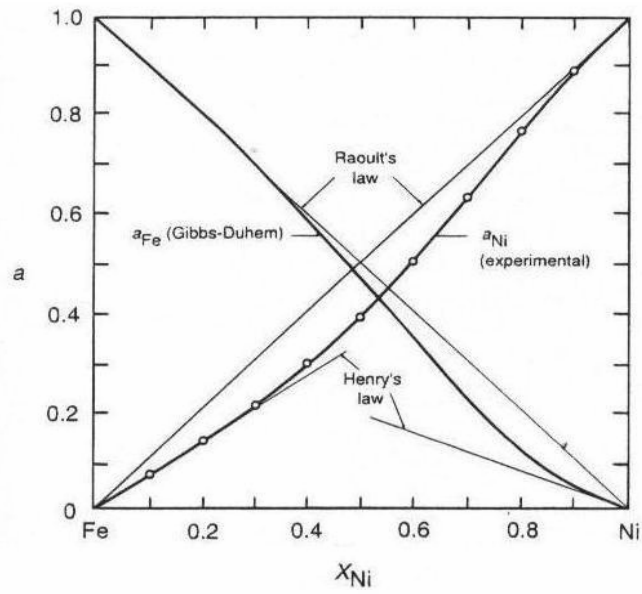


Figure 9.4 Activities in the system iron-copper at 1550 C (From J.P.Morris and G.R.Zellars , "Vapor Pressure of Liquid Copper and Activities in Liquid Fe-Cu Alloys," Trans. AIME (1956), vol. 206 , p.1086)

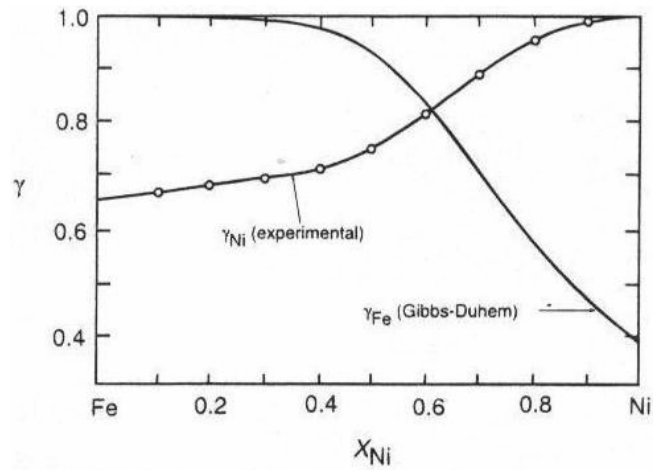


Figure 9.5 Activity coefficients in the system iron-nickel at 1600°C

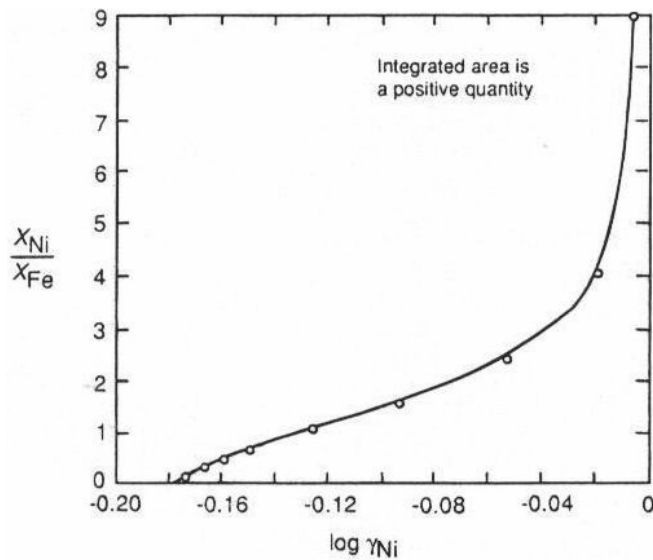


Figure 9.6 Application of the Gibbs-Duhem equation to determination of the activity of iron in the system iron-nickel

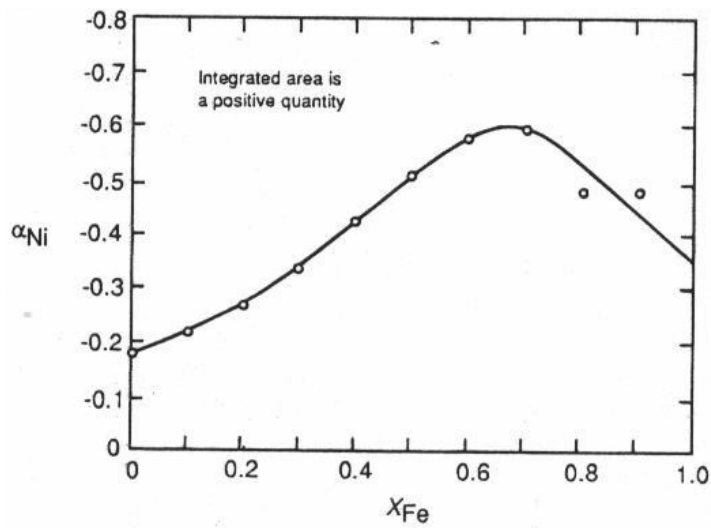


Figure 9.7 The variation of α_{Ni} with composition in the system iron-nickel

Ex 1: Fe-Ni alloy ($\gamma_{Ni} < 1$) $T = 1600$

$a_{Ni}(X_{Ni})$ is measured Fig. 9.4

$\gamma_{Ni}(X_{Ni})$ can be calculated Fig. 9.5

$\left(\frac{X_{Ni}}{X_{Fe}} \right)$ v.s. $\log \gamma_{Ni}$ Fig. 9.6
 $\alpha_{Ni}(X_{Fe})$ Fig. 9.7
 } calculate γ_{Fe}

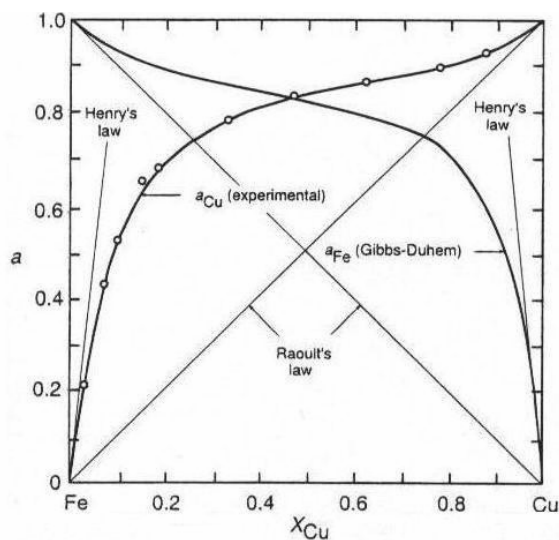


Figure 9.8 Activities in the system iron-copper at 1550 C (From J.P.Morris and G.R. Zellars, "Vapor Pressure of Liquid Copper and Activities in Liquid Fe-Cu Alloys," Trans. AIME (1956), vol. 206, p.1086)

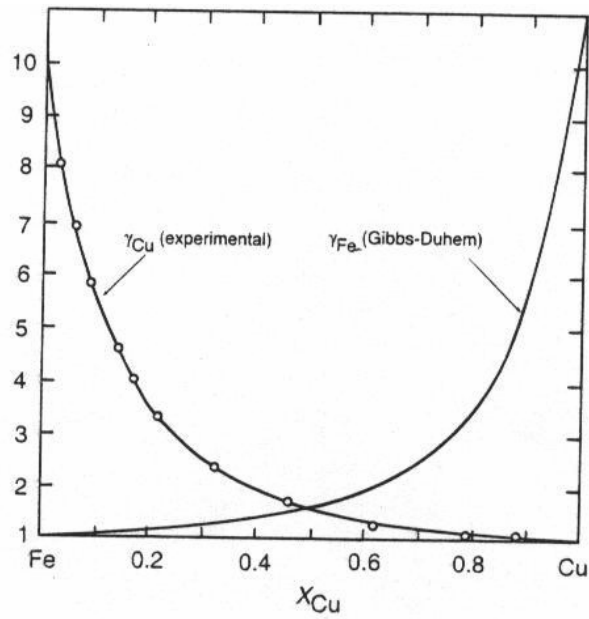


Figure 9.9 Activity coefficients in the system iron-copper at 1550°C

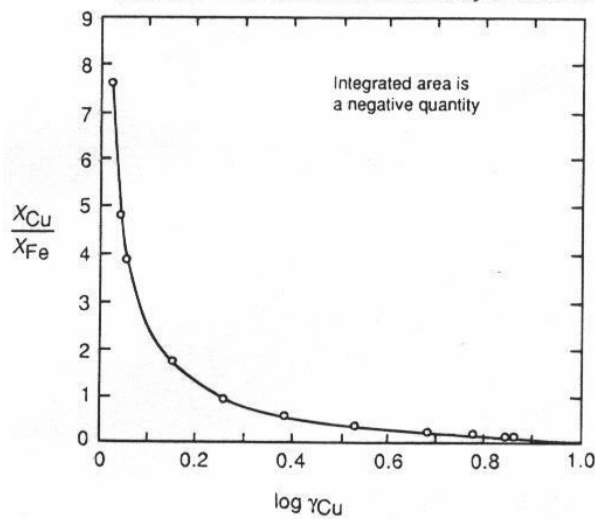


Figure 9.10 Application of the Gibbs-Duhem equation to determination of the activity of iron in the system iron-copper

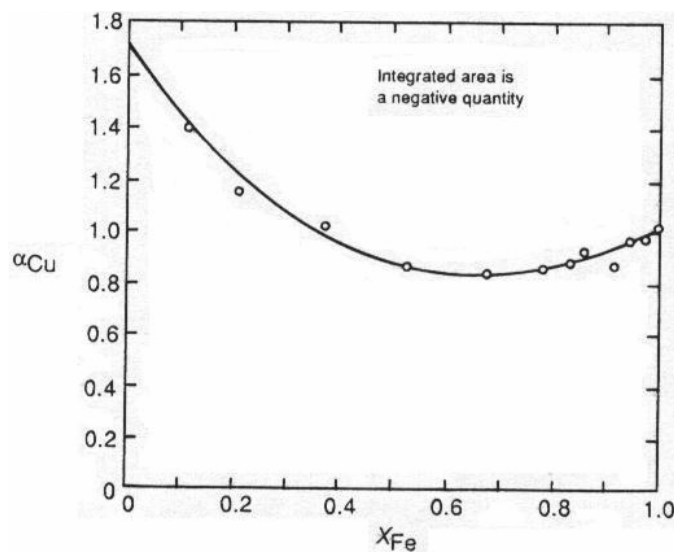


Figure 9.11 The variation of α_{Cu} with composition in the system iron-copper

Ex 2 : Fe-Cu alloy ($\gamma_{Cu} > 1$) T=1550

$a_{Cu}(X_{Cu})$ is measured Fig . 9.8

$\gamma_{Cu}(X_{Cu})$ can be calculated Fig . 9.9

$$\left. \begin{array}{l} \left(\frac{X_{Cu}}{X_{Fe}} \right) \text{ v.s. } \log \gamma_{Cu} \quad \text{Fig . 9.10} \\ \alpha_{Cu}(X_{Fe}) \quad \quad \quad \text{Fig . 9.11} \end{array} \right\} \text{calculate } \gamma_{Fe}$$

2. solute B obeys Henry's Law \Leftrightarrow solvent A obeys Raoult's Law

$$a_B = \gamma_B X_B, \quad \gamma_B = \text{constant} \quad a_A = X_A$$

proof: \ominus $a_B = \gamma_B X_B$

$$\therefore \ln a_B = \ln \gamma_B + \ln X_B$$

$$\therefore d \ln a_B = d \ln X_B$$

Gibbs-Duhem eq. $d \ln a_A = - \left(\frac{X_B}{X_A} \right) d \ln a_B$

$$\therefore d \ln a_A = - \frac{X_B}{X_A} d \ln X_B$$

$$= - \frac{X_B}{X_A} \frac{dX_B}{X_B}$$

$$= - \frac{dX_B}{X_A}$$

$$= \frac{dX_A}{X_A}$$

$$= d \ln X_A$$

$$\therefore \ln a_A = \ln X_A + c'$$

$$a_A = c X_A$$

But $X_A = 1$ (pure material)

$$a_A = 1, c = 1$$

$$a_A = X_A \text{ (Raoult's Law)}$$

3. Given $a_A(X_A)$, calculate ΔG^M

$$\Delta \overline{G}_A^M = \Delta G^M + X_B \frac{d\Delta G^M}{dX_A}$$

$$\frac{\Delta \overline{G}_A^M dX_A}{X_B^2} = \frac{-\Delta G^M dX_B + X_B d\Delta G^M}{X_B^2} = d \left(\frac{\Delta G^M}{X_B} \right)$$

$$\left(\frac{\Delta G^M}{X_B} \right) = \int_0^{X_A} \frac{\Delta \overline{G}_A^M dX_A}{X_B^2} \dots \dots \dots \text{Eq(1)}$$

$$\overline{\Delta G}_A^M = RT \ln a_A$$

$$\Delta G^M = RT X_B \int_0^{X_A} \frac{\ln a_A dX_A}{X_B^2} \dots \dots \dots \text{Eq(2)}$$

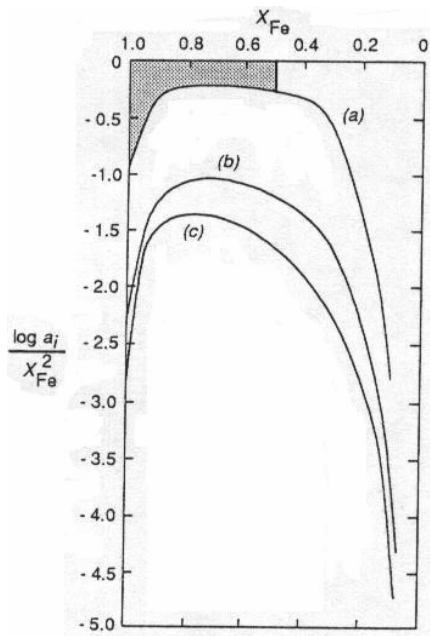
Ex 1: Fe-Ni alloy a_{Ni} measured

$$\Delta G^M = RT X_{Fe} \int_0^{X_{Ni}} \frac{\ln a_{Ni} dX_{Ni}}{X_{Fe}^2}$$

Ex 2: Fe-Cu alloy

$$\Delta G^M = RT X_{Fe} \int_0^{X_{Cu}} \frac{\ln a_{Cu} dX_{Cu}}{X_{Fe}^2}$$

Fig. 9-12, Fig. 9-13



a - $\log a_{Cu}/X_{Fe}^2$
 b - $\log X_i/(1 - X_i)^2$
 c - $\log a_{Ni}/X_{Fe}^2$
 shaded area = $\frac{(\Delta G^M \text{ at } X_{Fe} = 0.5)}{2.303 \times 8.3144 \times 1823 \times 0.5}$

Figure 9.12 Illustration of the direct calculation of the integral molar Gibbs free energies of mixing in the systems iron-copper at 1550°C and iron-nickel at 1600°C

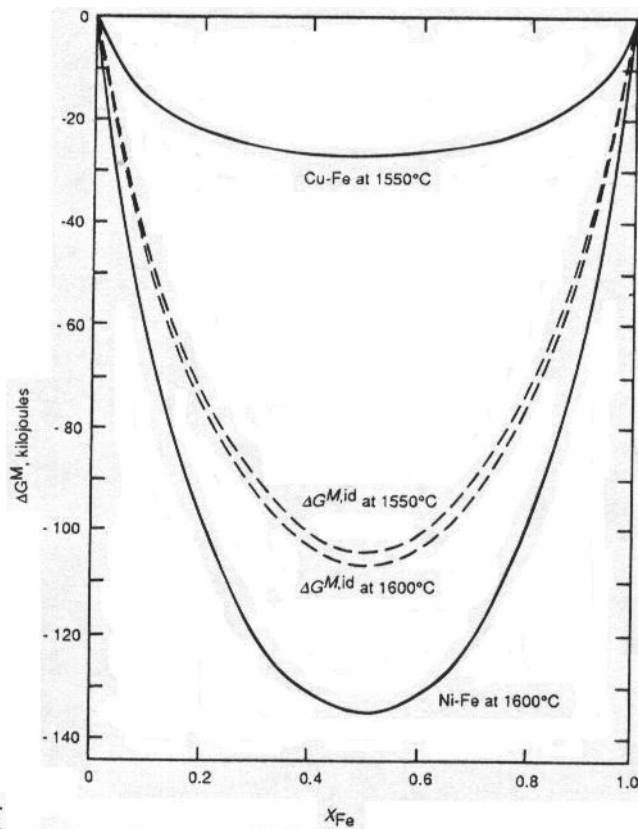


Figure 9.13 The integral molar Gibbs free energies of mixing in the systems iron-copper at 1550°C and iron-nickel at 1600°C

Notes:

1. when $X_i \rightarrow 0 \left[\frac{\ln a_i}{(1 - X_i)^2} \right] \rightarrow -\infty \therefore$ error exists

2. For ideal solution : $a_i = X_i$

$$\begin{aligned} \Delta G^M &= RT(1 - X_i) \int_0^{X_i} \frac{\ln X_i}{(1 - X_i)^2} dX_i \\ &= RT(1 - X_i) \left[\frac{X_i \ln X_i}{(1 - X_i)} + \ln(1 - X_i) \right] \\ &= RT [X_i \ln X_i + (1 - X_i) \ln(1 - X_i)] \end{aligned}$$

3. Eq.(1) can be used for any extensive properties

$$\left\{ \begin{aligned} \Delta H^M &= X_B \int_0^{X_A} \frac{\overline{\Delta H_A^M}}{X_B^2} dX_A \\ \Delta S^M &= X_B \int_0^{X_A} \frac{\overline{\Delta S_A^M}}{X_B^2} dX_A \end{aligned} \right.$$

$$4. \Delta G^{XS} = RT X_B \int_0^{X_A} \frac{\ln \gamma_A}{X_B^2} dX_A$$

when $X_i \rightarrow 0$, $\gamma_i \rightarrow \text{const.}$

$$\therefore \frac{\ln \gamma_i}{(1 - X_i)^2} \text{ is finite}$$

$\Delta G^M = \Delta G^{M,id} + \Delta G^{XS}$, error can be eliminated.

$$\Delta G^{M,id} = RT(X_A \ln X_A + X_B \ln X_B)$$

§ 9-9 Regular Solution

$$1. \text{ Ideal solution } \left\{ \begin{aligned} a_i &= X_i \\ \gamma_i &= 1 \end{aligned} \right. \left\{ \begin{aligned} \overline{\Delta H_i^M} &= 0 \\ \overline{\Delta S_i^M} &= -R \ln X_i \end{aligned} \right.$$

$$\text{Nonideal solution } : \left\{ \begin{aligned} a_i &\neq X_i \\ \gamma_i &\neq 1 \end{aligned} \right. \quad \overline{\Delta H_i^M} \neq 0$$

2. The Simplist Mathematical Form of a nonideal solution is "Regular solution".

⊗ Definition

$$\left\{ \begin{array}{l} (1) \Delta \bar{S}_i^M = \Delta \bar{S}_i^{M,id} = -R \ln X_i \\ (2) \Delta \bar{H}_i^M \text{ is a function of composition only. It is indep. of } T. \end{array} \right.$$

Consider that: $X_A > 0, X_B > 0$, then $H^M > 0$

Since H^M is a function of composition only, $H^M = H^M(X_B)$.

$$H^M = X_A X_B (a' + b X_B + c X_B^2 + d X_B^3 + \dots)$$

The simplest mathematical form of regular solution is $H^M = a' X_A X_B$

$$\text{If } \left\{ \begin{array}{l} RT \ln \gamma_B = a' X_A^2 \\ RT \ln \gamma_A = a' X_B^2, \quad a' \text{ is constant} \end{array} \right.$$

$$\text{From eq(9.61) } \ln g_A = - X_A X_B a_B - \int_{X_A=1}^{X_A} a_B dX_A$$

If a_B is indep. of composition

$$\begin{aligned} \Rightarrow \ln g_A &= - X_A X_B a_B - a_B (X_A - 1) \\ &= - X_A X_B a_B + a_B X_B \\ &= a_B X_B (1 - X_A) \\ &= a_B X_B^2 \end{aligned}$$

$$\text{By definition: } a_A = \frac{\ln g_A}{X_B^2}$$

$$\therefore a_B = a_A = a$$

$$\text{If } RT \ln g_A = a' X_B^2$$

$$\Rightarrow a = \frac{a'}{RT}$$

i.e. a function is an inverse function of temperature for the simplest regular solution

3. Excess Quantity

$$\ominus \quad \Delta \bar{G}_i = RT \ln a_i = RT \ln g_i + RT \ln X_i$$

$$\therefore \Delta \bar{G}_i = \Delta \bar{G}_i^{id} + \Delta \bar{G}_i^{xs}$$

$$\text{or } G = G^{id} + G^{xs} \quad (\text{one mole}), \quad \Delta G^M = \Delta G^{M,id} + G^{xs}$$

$$\Delta G^M = \Delta H^M - T \Delta S^M$$

$$\text{ideal solution : } \Delta H^{M,\text{id}} = 0, \Delta G^{M,\text{id}} = -T \Delta S^{M,\text{id}}$$

$$\begin{aligned} \therefore G^{\text{xs}} &= \Delta G^M - \Delta G^{M,\text{id}} \\ &= (\Delta H^M - T \Delta S^M) - (-T \Delta S^{M,\text{id}}) \\ &= \Delta H^M - T(\Delta S^M - \Delta S^{M,\text{id}}) \end{aligned}$$

$$\text{since for a regular solution } \Delta S^M = \Delta S^{M,\text{id}}$$

$$\Rightarrow G^{\text{xs}} = \Delta H^M$$

$$\Delta G^M = \sum X_i \Delta \overline{G}_i^M = X_A (RT \ln a_A + RT \ln a_B)$$

$$\begin{aligned} \Delta G^M &= RT(X_A \ln X_A + X_B \ln X_B) + RT(X_A \ln g_A + X_B \ln g_B) \\ \ominus \Delta G^{M,\text{id}} &= RT(X_A \ln X_A + X_B \ln X_B) \end{aligned}$$

$$\therefore G^{\text{xs}} = RT(X_A \ln g_A + X_B \ln g_B)$$

$$\therefore G^{\text{xs}} = X_A \overline{G}_A^{\text{xs}} + X_B \overline{G}_B^{\text{xs}}$$

For the simplest regular solution: $a_B = a_A = a$

$$\Rightarrow \ln g_A = a X_B^2, \quad \ln g_B = a X_A^2$$

$$\begin{aligned} \Rightarrow G^{\text{xs}} &= RT(X_A a X_B^2 + X_B a X_A^2) \\ &= a RT X_A X_B = a' X_A X_B \end{aligned}$$

For the simplest regular solution:

$$G^{\text{xs}} = \Delta H^M = a RT X_A X_B = a' X_A X_B$$

$$G^{\text{xs}} = \Delta H^M \text{ is indep. of } T$$

$$\left(\frac{\partial G^{\text{xs}}}{\partial T} \right)_{P,\text{comp}} = -S^{\text{xs}} = 0$$

at a fixed composition

$$\overline{G}_A^{\text{xs}} = RT_1 \ln g_{A(T_1)} = RT_2 \ln g_{A(T_2)} = a' X_B^2$$

$$\therefore \frac{\ln g_{A(T_2)}}{\ln g_{B(T_1)}} = \frac{T_1}{T_2}$$

Notes : (1) For the simplest regular solution

$$G^{\text{xs}} = \Delta H^M = a RT X_A X_B = a' X_A X_B$$

$\therefore a T$ is indep. of T

(2) If $\Delta H^M = b X_A X_B$, $G^{\text{xs}} = b' X_A X_B$, $b \neq b'$

$$\Rightarrow \Delta S^M \neq \Delta S^{M,id}$$

\Rightarrow Nonregular

e.g. (1) Au-Cu, 1550K $\left\{ \begin{array}{l} G^{xs} = -24060 X_{Cu} X_{Au} \\ \Delta H^M \text{ is asymmetric} \Rightarrow S^{xs} \neq 0 \end{array} \right.$

(2) Au-Ag, 1350K $\left\{ \begin{array}{l} \Delta H^M = -20590 X_{Ag} X_{Au} \\ G^{xs} \text{ is asymmetric} \Rightarrow S^{xs} \neq 0 \end{array} \right.$

§ 9-10 Statistical (Quasi-chemical) Model of

Solution

- Physical significance of a regular solution
- Assumptions : $\overline{V}_A = V_A^O = V_B^O = \overline{V}_B$, $\Delta V^M = 0$

\therefore Energy of solution \Leftrightarrow sum of interatomic bond energies.

Consider : (N_A A atoms + N_B B atoms)

$$N_A + N_B = N_o \quad (1 \text{ mole})$$

$$\Rightarrow X_A = \frac{N_A}{N_A + N_B} = \frac{N_A}{N_o}, \quad X_B = \frac{N_B}{N_o}$$

$$\therefore E = P_{AA} E_{AA} + P_{BB} E_{BB} + P_{AB} E_{AB}$$

E_{AA} , E_{BB} , E_{AB} are bond energies of A-A, B-B, A-B, respectively.

P_{AA} , P_{BB} , P_{AB} are bond numbers of A-A, B-B, A-B, respectively.

$$N_A Z = P_{AB} + 2P_{AA}$$

$$\therefore P_{AA} = \frac{1}{2} (N_A Z - P_{AB}), \quad \text{similarly } P_{BB} = \frac{1}{2} (N_B Z - P_{AB})$$

$$\therefore E = \frac{1}{2} N_A Z E_{AA} + \frac{1}{2} Z N_B E_{BB} + P_{AB} [E_{AB} - \frac{1}{2} (E_{AA} + E_{BB})]$$

For pure N_A A atoms : $N_A Z = 2P_{AA}$

Pure N_B B atoms : $Z N_B = 2P_{BB}$

$$\text{Before mixing : } E_o = \frac{1}{2} N_A Z E_{AA} + \frac{1}{2} Z N_B E_{BB}$$

$$\Delta E^M = E - E_o = P_{AB} [E_{AB} - \frac{1}{2} (E_{AA} + E_{BB})]$$

$$\ominus \quad \Delta H^M = \Delta E^M + P \Delta V^M = \Delta E^M \quad (\Delta V^M = 0)$$

$$\therefore \Delta H^M = \Delta E^M = P_{AB} [E_{AB} - \frac{1}{2}(E_{AA} + E_{BB})]$$

For solutions which exhibit relatively small deviations from ideal behavior,

$$\text{i.e. } |\Delta H^M| \leq RT$$

\therefore mixing of atoms can be assumed to be random

P_{AB} can be calculated .

Consider two neighboring lattice sites **a b**

$$\text{Probability that } \left\{ \begin{array}{l} \mathbf{a} \text{ occupied by A and} \\ \mathbf{b} \text{ occupied by B} \end{array} \right\} X_A X_B$$

$$\text{Probability that } \left\{ \begin{array}{l} \mathbf{a} \text{ occupied by B and} \\ \mathbf{b} \text{ occupied by A} \end{array} \right\} X_B X_A$$

\therefore Probability that a neighboring pair of sites contains A-B pair is $2 X_A X_B$

\therefore (number of A-B bonds) = (number of neighboring pair of sites) \times (Probability of A-B pair)

$$\therefore P_{AB} = \left(\frac{1}{2} Z N_o\right) \times (2 X_A X_B) = Z N_o X_A X_B$$

$$\text{i.e. } \Delta H^M = Z N_o X_A X_B [E_{AB} - \frac{1}{2}(E_{AA} + E_{BB})]$$

$$\text{define } \boxed{\Omega \equiv Z N_o [E_{AB} - \frac{1}{2}(E_{AA} + E_{BB})]}$$

$$\Rightarrow \Delta H^M = \Omega X_A X_B$$

Since random mixing is assumed, statistical model \Leftrightarrow regular solution model

$$\therefore \Delta H^M = G^{xs} = \Omega X_A X_B = RT \mathbf{a} X_A X_B$$

$$\Rightarrow \boxed{\mathbf{a} = \frac{\Omega}{RT}} \quad \text{i.e. } \boxed{\mathbf{a}' = \Omega}$$

$$\begin{aligned} \ominus \quad \overline{\Delta H}_A^M &= \Delta H^M + (1 - X_A) \frac{d\Delta H^M}{dX_A} \\ &= \Omega X_A X_B + X_B \Omega (X_B - X_A) = \Omega X_B^2 \end{aligned}$$

$$\text{similarly, } \overline{\Delta H}_B^M = \Omega X_A^2$$

$$\ominus \quad \text{Mixing is random } \therefore \begin{cases} \overline{\Delta S}_A^M = -R \ln X_A \\ \overline{\Delta S}_B^M = -R \ln X_B \end{cases}$$

$$\therefore \overline{\Delta G}_A^M = \overline{\Delta H}_A^M - T \overline{\Delta S}_A^M$$

$$= \Omega X_B^2 + RT \ln X_A$$

But $\Delta \overline{G}_A^M = RT \ln a_A = RT \ln g_A + RT \ln X_A$

$$\Rightarrow RT \ln g_A = \Omega X_B^2$$

$$\Rightarrow \ln g_A = \frac{\Omega}{RT} X_B^2 = a X_B^2, \quad \text{similarly} \quad \ln g_B = \frac{\Omega}{RT} X_A^2 = a X_A^2$$

Note: (1) Ideal solution ,

$$\Delta H^M = 0, \text{ i.e. } \Omega = 0, \quad E_{AB} = \frac{1}{2}(E_{AA} + E_{BB})$$

(2) Negative deviation

$$\Delta H^M < 0, \text{ i.e. } \Omega < 0, \quad |E_{AB}| > \frac{1}{2}(E_{AA} + E_{BB}), \quad g_i < 1$$

(3) Positive deviation

$$\Delta H^M > 0, \text{ i.e. } \Omega > 0, \quad |E_{AB}| < \frac{1}{2}(E_{AA} + E_{BB}), \quad g_i > 1$$

(4) Henry's Law : $X_B \rightarrow 1 \quad X_A \rightarrow 0$

$$\ln g_A \rightarrow \ln g_A^o = \frac{\Omega}{RT} \quad \text{or} \quad g_A^o = e^{\frac{\Omega}{RT}}$$

(5) when $|E_{AB}|$ is significantly greater or less than $\frac{1}{2} |E_{AA} + E_{BB}|$

$$\Rightarrow |\Omega| \text{ increases}$$

\Rightarrow Random mixing cannot be assumed.

\Rightarrow Applicability of statistical model decreases .

(6) Equilibrium configuration of a solution at constant T, P $\Leftrightarrow G = G_{\min}$

$$\Theta G = H - TS \quad \therefore G_{\min} \Leftrightarrow H_{\min} \text{ and } S_{\max}$$

⊗ If $|E_{AB}| > \frac{1}{2} |E_{AA} + E_{BB}|$ (Negative deviation)

$$\Omega < 0, \quad \Delta H^M < 0, \quad H < 0$$

$$H_{\min} \Leftrightarrow P_{AB} \rightarrow (P_{AB})_{\max}$$

i.e. $|\Omega|$ increases $\Rightarrow P_{AB}$ increases (ordering)

⊗ If $S \rightarrow S_{\max}$, completely random mixing

$$T \text{ increases} \Rightarrow (TS) \uparrow \Rightarrow G \downarrow$$

$\therefore G \rightarrow G_{\min}$ is compromised between Ω and T

\therefore when T is not too high and Ω is appreciably negative

$$\Rightarrow P_{AB} > P_{AB}(\text{random})$$

\Rightarrow Assumption of random mixing is not valid

⊗ For a given $\Omega : T \uparrow \Rightarrow$ more nearly random mixing

For a given $T : |\Omega| \downarrow \Rightarrow$ more nearly random mixing

⊗ only when $\Delta H^M = 0$, random configuration is the equilibrium

i.e. $\Delta G^M = \Delta G_{\min}^M$ (random)

⊗ At constant T , as $|\Omega| \uparrow \Rightarrow \Delta G_{\min}^M$ moves far away from random

if $\Delta H^M < 0$, $\Delta G_{\min}^M \rightarrow$ ordered

if $\Delta H^M > 0$, $\Delta G_{\min}^M \rightarrow$ clustered

⊗ At constant $|\Omega|$, as $T \uparrow \Rightarrow |T\Delta S^M| \uparrow$

$\Rightarrow \Delta G_{\min}^M$ moves toward center (random)

§ 9-11 Subregular Solution

⊗ Simplest regular solution :

$$\Omega = \mathbf{a}' = \frac{\mathbf{a}}{RT} = ZN_o [E_{AB} - \frac{1}{2}(E_{AA} + E_{BB})] = \text{constant}$$

$$\text{and } G^{xs} = \Delta H^M = \mathbf{a}' X_A X_B = \Omega X_A X_B$$

\therefore parabolic function, symmetric about $X_A = X_B = 0.5$

⊗ Subregular Solution

$$G^{xs} = \Delta H^M = (a + b X_B) X_A X_B$$

constants a, b have no physical meaning, they are parameters adjusted to fit equation to experimentally measured data

e.g. Ag-Au at $T = 1350$ K

data fitting $a = -11320$ J, $b = 1940$ J

⊗ Non-regular Solution

G^{xs} is a function of X_B, T

ΔH^M is also a function of X_B, T

$\Delta S^M \neq \Delta S^{M,id}$ ($S^{xs} \neq 0$)

$$\text{e.g. } G^{xs} = (a_o + b_o X_B) X_A X_B \left(1 - \frac{T}{t}\right)$$

$$\therefore S^{xs} = - \left(\frac{\partial G^{xs}}{\partial T} \right) = \frac{(a_o + b_o X_B) X_A X_B}{t}$$

$$\Delta H^M = G^{xs} + T S^{xs} = (a_o + b_o X_B) X_A X_B$$

EX1. Cu-Au solid solution at $T=600^{\circ}\text{C}=873\text{ K}$

Solution is regular with $G^{xs} = -28280 X_{\text{Au}} X_{\text{Cu}} \text{ J}$

For pure Cu and Au

$$\ln p_{\text{Cu}}^{\circ} (\text{atm}) = -\frac{40920}{T} - 0.86 \ln T + 21.67$$

$$\ln p_{\text{Au}}^{\circ} (\text{atm}) = -\frac{45650}{T} - 0.306 \ln T + 10.81$$

calculate p_{Cu} and p_{Au} over Cu-Au solid solution at $X_{\text{Cu}}=0.6$, $T=873\text{ K}$

Sol: Θ Regular solution $\therefore \Omega = -28280 \text{ J}$

$$\ln g_{\text{Cu}} = \frac{\Omega}{RT} X_{\text{Au}}^2, \quad \ln g_{\text{Au}} = \frac{\Omega}{RT} X_{\text{Cu}}^2$$

$$\therefore g_{\text{Cu}} = 0.536, \quad g_{\text{Au}} = 0.246$$

$$\left. \begin{aligned} a_{\text{Cu}} &= g_{\text{Cu}} X_{\text{Cu}} = 0.322 \\ a_{\text{Au}} &= g_{\text{Au}} X_{\text{Au}} = 0.098 \end{aligned} \right\}$$

By definition:

$$a_{\text{Cu}} \equiv \frac{p_{\text{Cu}}}{p_{\text{Cu}}^{\circ}}$$

$$a_{\text{Au}} \equiv \frac{p_{\text{Au}}}{p_{\text{Au}}^{\circ}}$$

$$\text{at } T=873\text{ K} \quad p_{\text{Cu}}^{\circ} = 3.35 \times 10^{-14} \text{ atm}$$

$$p_{\text{Au}}^{\circ} = 1.52 \times 10^{-16} \text{ atm}$$

$$\therefore p_{\text{Cu}} = 1.08 \times 10^{-14} \text{ atm}$$

$$p_{\text{Au}} = 1.50 \times 10^{-16} \text{ atm}$$

EX2. Ga-Cd Liquid solution at $T=700\text{K}$

Regular solution, $X_{\text{Ga}} = 0.5$ $a_{\text{Ga}} = 0.79$

$$\Delta H_{\text{evap,Ga}} = 270,000 \text{ J/mole} \quad Z_{\text{Ga}} = 11$$

$$\Delta H_{\text{evap,Cd}} = 100,000 \text{ J/mole} \quad Z_{\text{Cd}} = 8$$

Calculate $E_{\text{Ga-Cd}} = ?$

Sol: $\ominus \quad g_{\text{Ga}} = \frac{a_{\text{Ga}}}{X_{\text{Ga}}} = 1.59$

$$\ln g_{\text{Ga}} = \frac{\Omega}{RT} X_{\text{Cd}}^2$$

$$\therefore \Omega = 10795 \text{ J/mole}$$

$$\Omega = Z N_o [E_{\text{Ga-Cd}} - \frac{1}{2}(E_{\text{Ga-Ga}} + E_{\text{Cd-Cd}})]$$

$$\ominus \text{ liquid Ga : } \Delta H_{\text{evap,Ga}} \cong - \frac{1}{2} Z_{\text{Ga}} N_o E_{\text{Ga-Ga}}$$

$$\text{liquid Cd : } \Delta H_{\text{evap,Cd}} \cong - \frac{1}{2} Z_{\text{Cd}} N_o E_{\text{Cd-Cd}}$$

$$\therefore E_{\text{Ga-Ga}} = - 8.15 \times 10^{-20} \text{ J}$$

$$E_{\text{Cd-Cd}} = - 4.15 \times 10^{-20} \text{ J}$$

$$\text{Assume : Ga-Cd liquid } Z = \frac{1}{2} (Z_{\text{Ga}} + Z_{\text{Cd}}) = 9.5$$

$$\therefore E_{\text{Ga-Cd}} = - 5.96 \times 10^{-20} \text{ J}$$